

Project “SLiT-J”

Synchrotron Light in Tohoku, Japan

Outline

Conceptual Design of Accelerator Complex V1.0

April, 2014

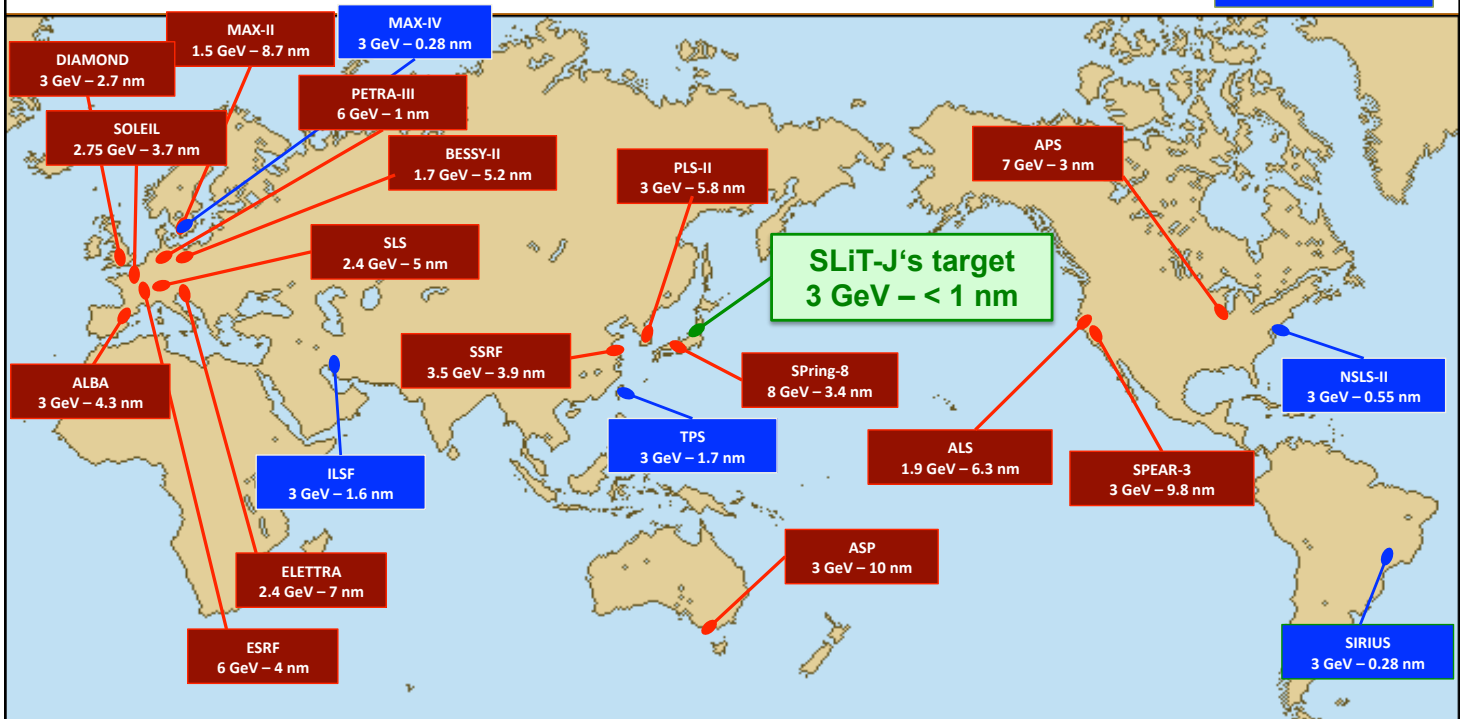
SLiT-J Design Team

High Brilliant Light Source in the World

horizontal emittance $\mathcal{E}_x < 10$ nrad

Operational

Under constructing



Synchrotron integrals

$$I_1 = \oint \frac{\eta_x}{\rho} ds$$

$$I_2 = \oint \frac{1}{\rho^2} ds$$

$$I_3 = \oint \frac{1}{|\rho|^3} ds$$

$$I_4 = \oint \frac{\eta_x}{\rho} \left(\frac{1}{\rho^2} + 2K \right) ds$$

$$I_5 = \oint \frac{H}{|\rho|^3} ds \text{ where } H(s) = \gamma\eta^2 + 2\alpha\eta\eta' + \beta\eta'^2$$

Important function of quantum excitation in bends

1. Momentum compaction factor $\alpha = \frac{I_1}{2\pi R}$
2. Horizontal emittance $\epsilon_x = \frac{C_q \gamma^2 I_5}{(I_2 - I_4)}$ where $C_q = \frac{55}{32\sqrt{3}} \frac{\hbar}{mc} = 3.83 \times 10^{-13}$
3. Energy spread $\left(\frac{\sigma_E}{E}\right)^2 = \frac{C_q \gamma^2 I_3}{(2I_2 + I_4)}$
4. Energy loss $U_0 \approx \frac{C_\gamma E^4 I_2}{2\pi}$ where $C_\gamma = \frac{4\pi}{3(mc^2)^3} = 8.85 \times 10^{-5} \frac{m}{(GeV)^3}$
5. Damping partition $J_x = 1 - \frac{I_4}{I_2}$, $J_E = 2 + \frac{I_4}{I_2}$, $D = \frac{I_4}{I_2}$

How to achieve low emittance lattice

Theoretical minimum emittance

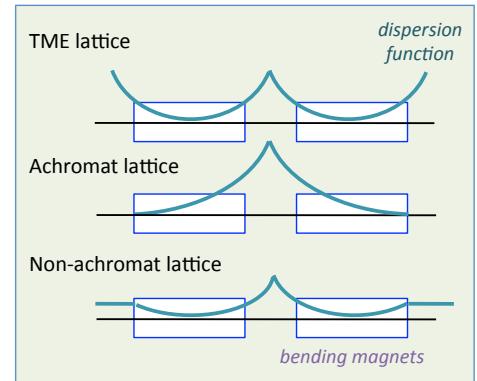
$$\epsilon_x^{\min} = \frac{1}{4\sqrt{15}} \frac{C_q \gamma^2 \theta^3}{J_x} (\text{achromat}), \quad \epsilon_x^{\min} = \frac{1}{12\sqrt{15}} \frac{C_q \gamma^2 \theta^3}{J_x} (\text{non-achromat})$$

$$C_q = 3.83 \times 10^{-13} \text{ (mrad)}$$

θ ; bending angle (rad)

J_x ; horizontal damping partition (~1.5)

$$J_x = 1 - \frac{\oint (1-2n)\eta/\rho^3 ds}{\oint 1/\rho^2 ds}$$



$$\epsilon_{x\text{-effective}} = \epsilon_x \sqrt{1 + \frac{\left(\eta_x \frac{\sigma_E}{E}\right)^2}{\epsilon_x \beta_x}}$$

- Smaller θ means increase of **number of bending magnets**.
- **Non-achromat lattice** reduces the emittance significantly.
 - ☞ Be careful, energy spread increases the effective emittance.

Reducing emittance further

$$\epsilon_x = C_q \gamma^2 \frac{I_5}{I_2 - I_4} \quad \text{- for radiation damping on bending magnets only}$$

$$\epsilon_{xw} = C_q \gamma^2 \frac{I_5 + I_{5w}}{I_2 - I_4 + I_{2w} - I_{4w}} \quad \text{- for radiation damping in bending magnets and wigglers (w denotes S.I. in wigglers)}$$

- Strong **damping wiggler** is employed in NSLS-II (2.1 nrad -> 0.55 nrad)

when $\frac{\langle H_{dipole} \rangle}{H_w} \gg 1$ $\epsilon_{xw} \approx \epsilon_x \frac{U_0}{U_0 + U_w}$ where U_0 ; Radiated power from dipoles
 U_w ; Radiated power from wigglers

$$U_0 \text{ [MW]} = 8.846 \times 10^{-2} E^4 \text{ [GeV]} / \rho \text{ [m]} I \text{ [A]}$$

$$U_w \text{ [MW]} = 6.336 \times 10^{-6} E^2 \text{ [GeV]} B_0^2 \text{ [kG]} L_w \text{ [m]} I \text{ [A]}$$

$$\epsilon_{xw} \approx \frac{1}{4} \epsilon_x \quad \Rightarrow \quad U_0 \approx 3U_w \quad \text{Bends; } E = 3 \text{ GeV, } \rho = 25 \text{ m}$$

$$U_0 \sim 0.3 \text{ MW/A}$$

$$\Rightarrow \quad \text{Wigglers; } E = 3 \text{ GeV, } B_0 = 1.5 \text{ T, } L_w = 70 \text{ m}$$

$$U_0 \sim 0.9 \text{ MW/A}$$

It is possible !

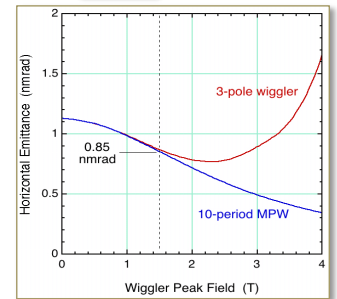
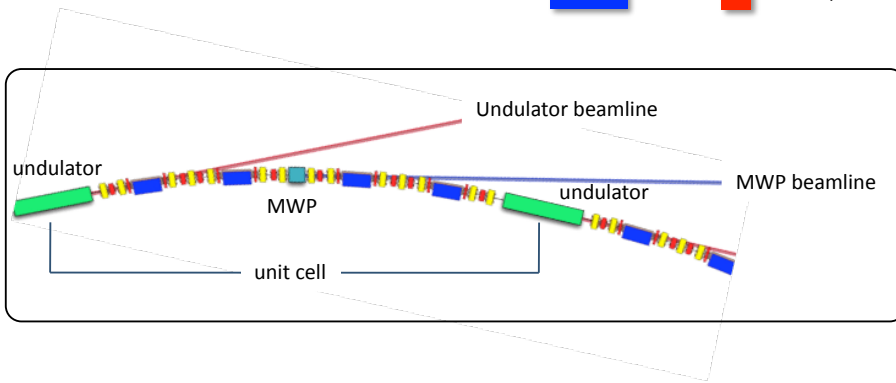
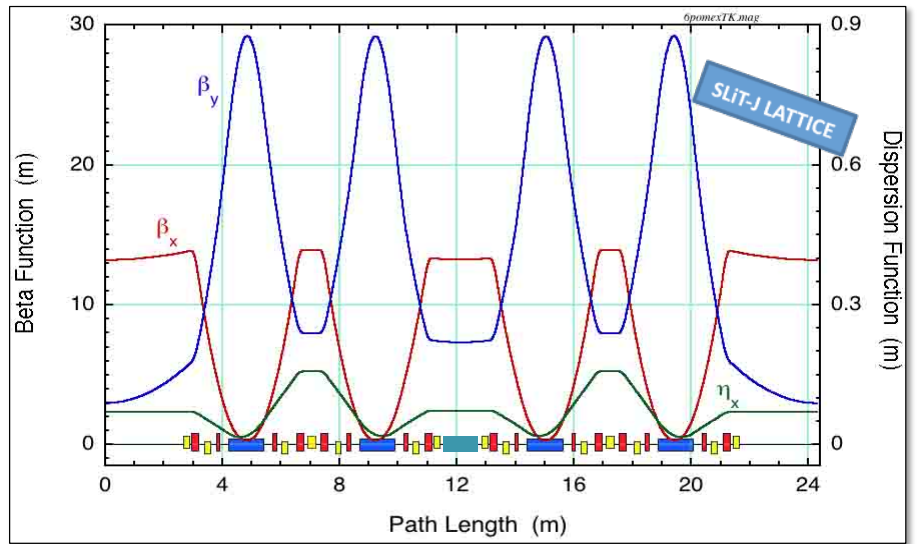
SLIT-J's solution: Multi-bend lattice structure + high-field multi-pole wiggler (MPW)

•SLIT-J 's Targets

- 1 $\epsilon_{\text{effective}} \sim 1 \text{ nrad}$ or below for world class high brilliant light source
- 2 $C \sim 300 - 400 \text{ m}$ for compactness and low construction and operation costs
- 3 More than 10 straight sections for sufficient number of the beam-lines

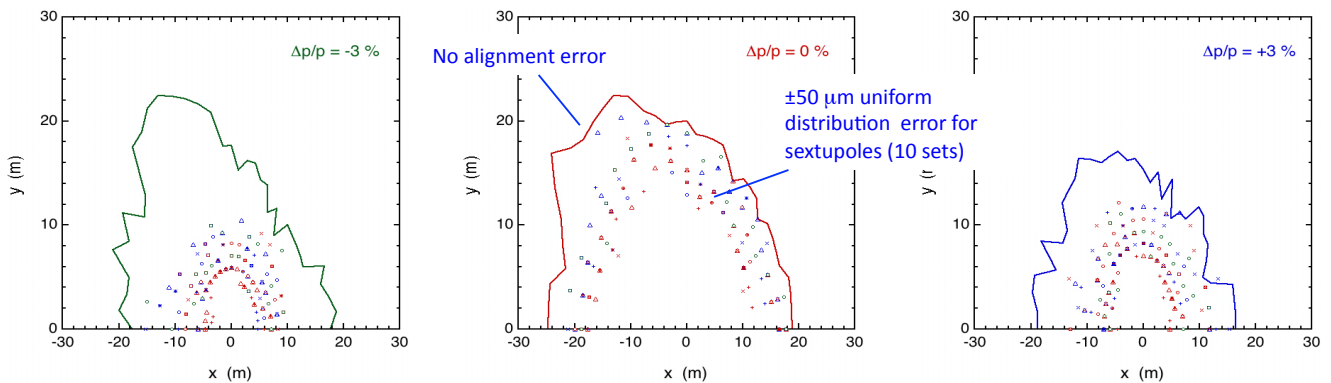
4-bend non-achromat lattice

- beam energy 2.998 GeV
- number of cells 14
- circumference 340 m
- number of bends 56 (combined)
B = 0.923455 T
K = 6.2 T/m
- number of quads 224 (5-family)
- number of sexts 196 (6-family)
- natural emittance 1.13 nrad
(with MPW) 0.85 nrad
- straight section 1.43 m × 14
5.33 m × 14



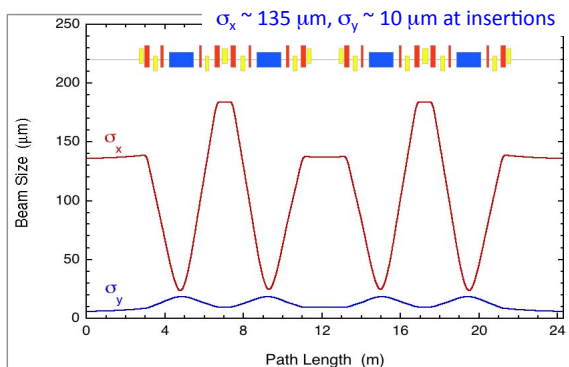
Additional damping effect by wiggler in short straight section

Dynamic aperture optimized by "Genetic Algorithm"

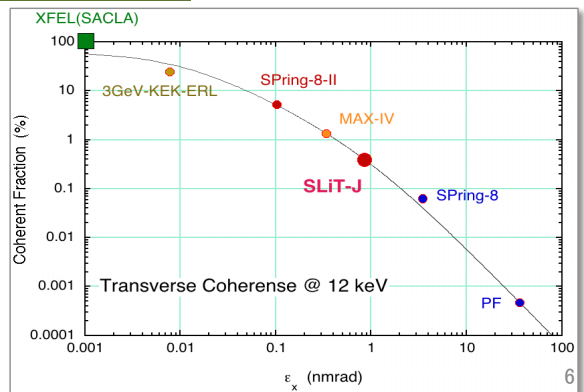


• Sufficiently wider dynamic aperture with reasonable sextupole strengths.

Beam size in a cell



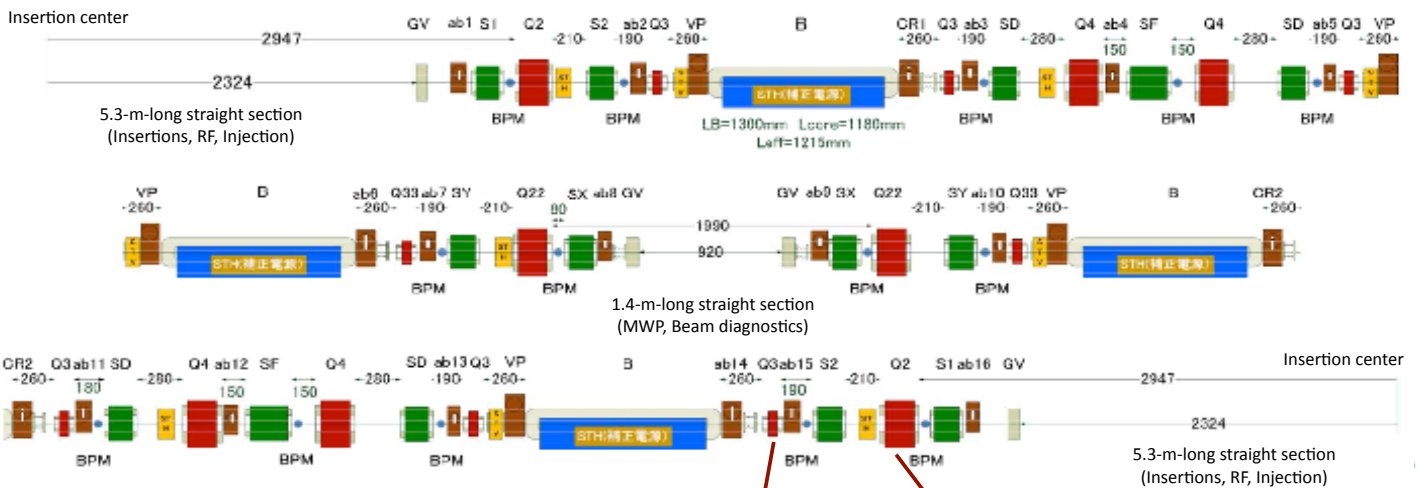
Coherent fraction



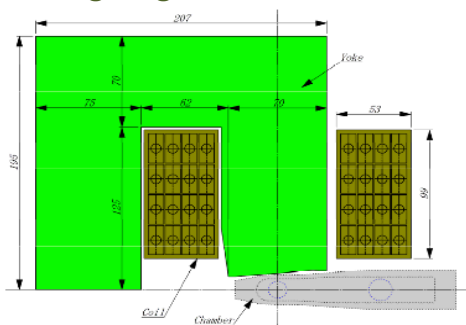
		(14-cell lattice)	(16-cell option)
Beam energy	E	2.998 GeV	2.998 GeV
Lattice structure		4-bend cell	4-bend cell
Circumference	C	339.92 m	388.480m
Number of cells (bends)	N_c	14 (56)	16 (64)
Long straight section	LSS	5.33 m × 14	5.33 m × 14
Short straight section	SSS	1.43 m × 14	1.43 m × 14
Betatron tune	(ν_x, ν_y)	(25.85, 6.75)	(29.15, 7.25)
Natural chromaticity	(ξ_x, ξ_y)	(-64.8, -44.7)	(-65.2, -47.5)
Natural horizontal emittance	ϵ_x	1.129 (0.85*) nmrad	0.78 (0.55*) nmrad
Momentum compaction factor	α	0.00047	0.00037
Natural energy spread	σ_E/E	0.0858 %	0.0805 %
Lattice functions at LSS	$(\beta_x, \beta_y, \eta_x)$	(13.2, 2.96, 0.07) m	(11.9, 3.73, 0.06) m
Damping partition number	(D, J_x, J_s)	(-0.341, 1.341, 1.659)	(-0.349, 1.349, 1.651)
Damping time	(τ_x, τ_y, τ_s)	(7.7, 10.3, 6.2) ms	(9.9, 13.4, 8.1) ms
Energy loss in bends	U_0	0.662 MeV/turn	0.579 MeV/turn
RF frequency	f_{RF}	508 MHz	508 MHz
RF voltage	V_{RF}	3 MV	3 MV
Harmonic number	h	576	658
Natural bunch length	σ_B	3.43 mm (11.1 ps)	2.95 mm (9.85 ps)

* with MPWs in all short straight section

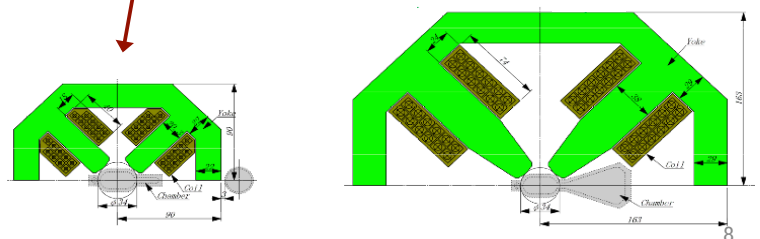
Magnet configuration (1 cell)



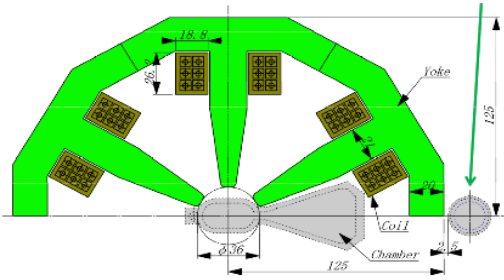
Bending magnet



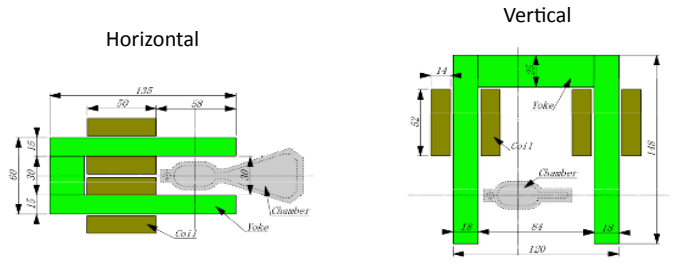
Quadrupole magnet



Sextupole magnet



Steering magnet



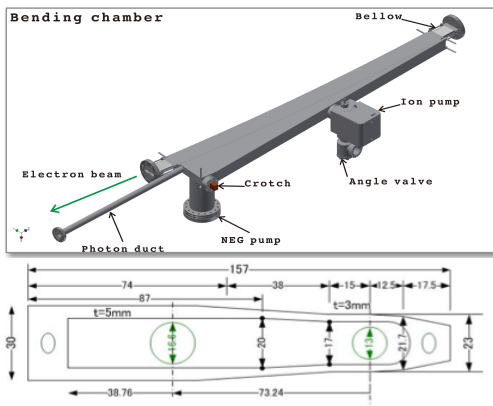
Power supply maximum rating

	Name	Magnet (number)	I_{max} (A)	Cable size sq, Length (m)	Total resistance (Ω)	Total voltage (V)	Power (kW)	Number of PS
Bend.	PS-B	B (56)	583	250 x 2, 1620	0.44 + 0.06 = 0.50	292	170.2	1
	PS-QA	QA (28)	306	250, 1200	0.15 + 0.10 = 0.25	77	23.4	2
Quad.	PS-QB	QB (56)	306	250, 1620	0.30 + 0.13 = 0.43	132	40.3	1
	PS-QC	QC (28)	192	150, 1200	0.11 + 0.16 = 0.27	51.8	10.0	1
	PS-QD	QD (84)	115	150, 2040	0.62 + 0.27 = 0.89	102.4	11.8	1
Sext.	PS-SXA	SXA (28)	129	100, 1200	0.23 + 0.24 = 0.47	60.0	7.8	6
	PS-SXB	SXB (28)	129	100, 1200	0.33 + 0.24 = 0.57	73.5	9.5	1

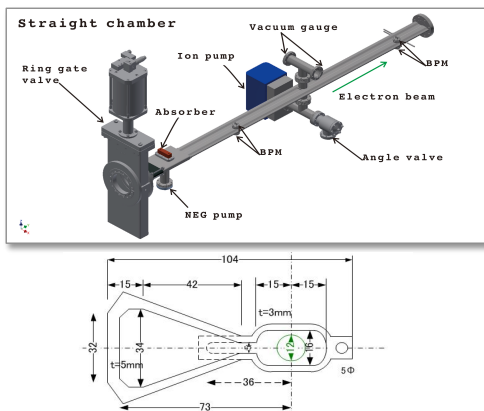
Sum 0.28 MW

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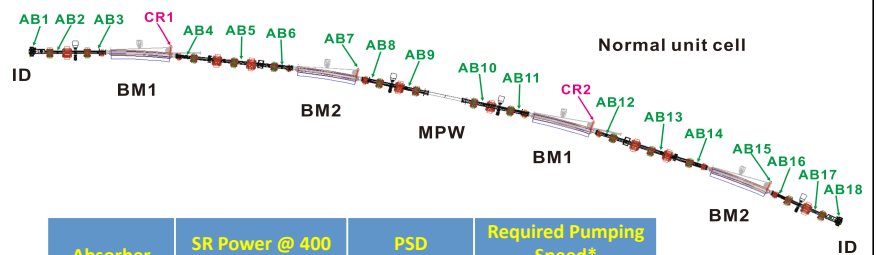
Bending magnet section



Straight section



Absorber and pumping speed in a cell

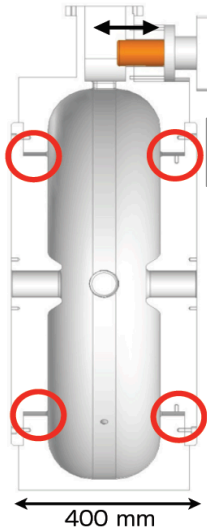


Absorber	SR Power @ 400 mA (W)	PSD (Pa/Ls)	Required Pumping Speed* (L/s)
AB1	337	5.1E-6	51
AB2	5	8.0E-8	1
AB3	11	1.7E-7	2
CR1	2619	4.0E-5	395
AB4	1069	1.6E-5	161
AB5	659	1.0E-5	100
AB6	231	3.5E-6	35
AB7	2755	4.2E-5	416
AB8	956	1.4E-5	144
AB9	748	1.1E-5	113
AB10	287	4.3E-6	43
AB11	44	6.6E-7	7
CR2	2679	4.0E-5	405
AB12	1067	1.6E-5	161
AB13	661	1.0E-5	100
AB14	231	3.5E-6	35
AB15	2755	4.2E-5	416
AB16	956	1.4E-5	144
AB17	772	1.2E-5	117
AB18	30	4.6E-7	5
Total	18873	2.850E-4	2850

* target pressure is 1e-7 Pa

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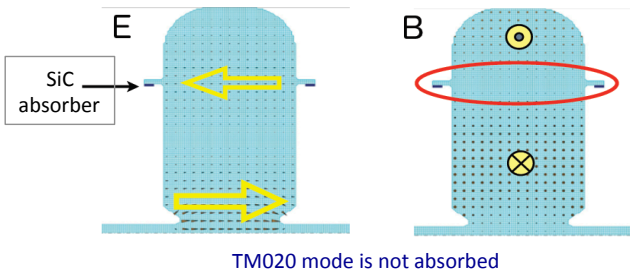
TM020 cavity (under developing)



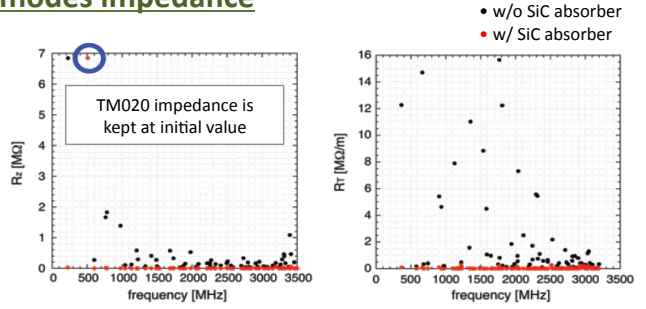
Coupling tuner $\beta = 1 \sim 3$

HOM•LOM absorber SiC slot

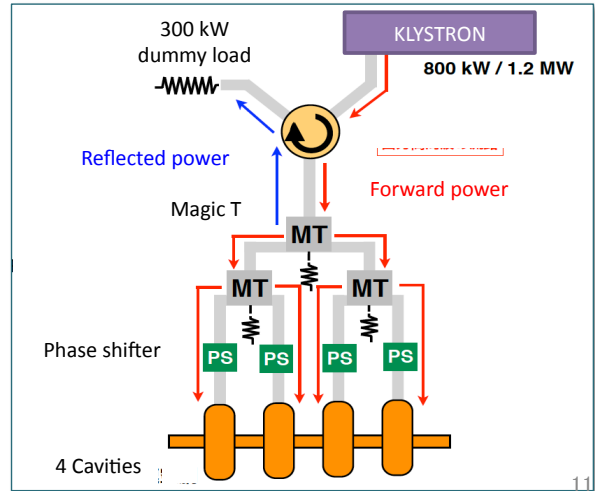
	Calculated (MAFIA)
f (MHz)	508.58
Mode	TM020
Q_0	60300
R_z (M Ω)	6.8
R_z/Q_0	113
V_a (MV)	0.75@83kW



Parasitic modes impedance



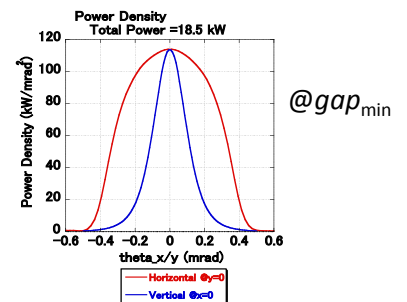
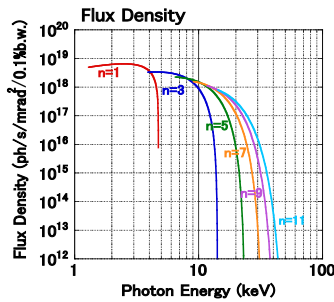
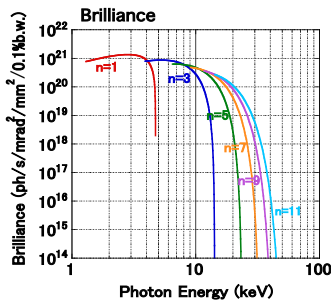
RF system



Hard X-ray

Lifetime due to residual gas scattering is more than 20 hours @ $< 1 \times 10^{-7}$ Pa

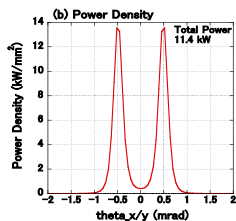
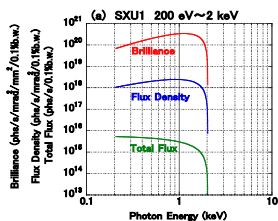
	λ_u (mm)	N_u	K_{max}	gap_{min} (mm)	ϵ_{photon} (keV)	Brilliance	Type, polarization
HXU	18	241	2.3	3.1	1 - 20	$\sim 10^{21}$ @several keV	In-vacuum, Linear



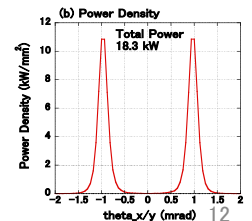
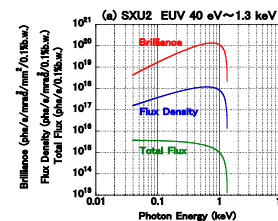
Soft X-ray

	λ_u (mm)	N_u	K_{max}	gap_{min} (mm)	ϵ_{photon} (keV)	Brilliance	Type, polarization
SXU1	42	104	2.97	15	0.2 - 2	$\sim 10^{20}$ @1keV	Helical
SXU2	64	68	5.74	18	0.04 - 1.3	$\sim 10^{20}$ @1keV	Helical

SXU1

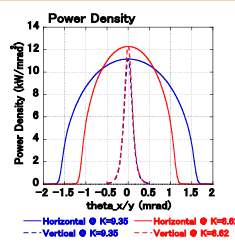
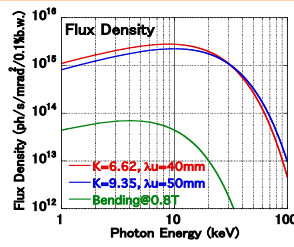
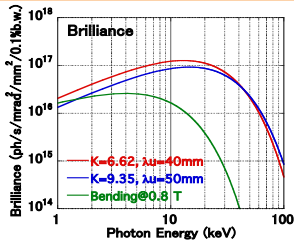


SXU2



MPW for hard-X continuum

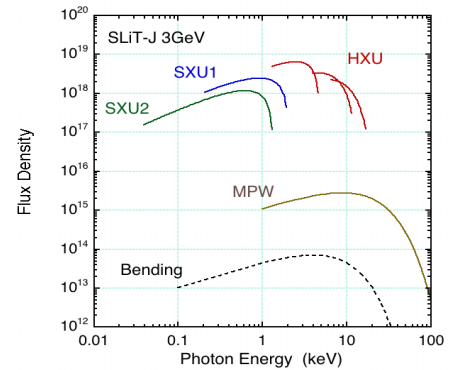
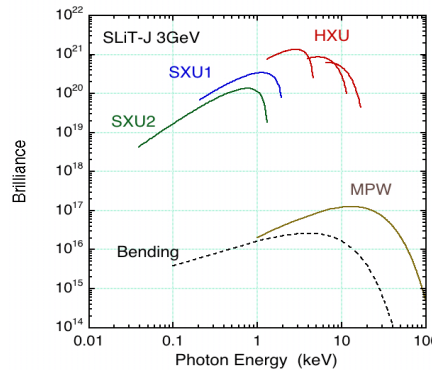
	λ_u (mm)	N_u	K_{max}	gap _{min} (mm)	ϵ_{photon} (keV)	Brilliance	Type, polarization
MPW	40	20	6.62	4.8	- 100	$\sim 10^{17}$ @several 10s keV	In-vacuum, Linear
MPW*	50	16	9.35	4.8	- 100	$\sim 10^{17}$ @several 10s keV	In-vacuum, Linear
MPW*	80	10	11.205	fixed 15	- 100	$\sim 10^{16}$ @several 10s keV	Damping W., Linear



*not yet confirmed

Summary

- Typical insertion devices are proposed. Details may change due to beamline applications.
- MPW will be used as substitute for bending magnet. Though damping effect to reduce the emittance is expected, MPW's parameter is not yet confirmed.

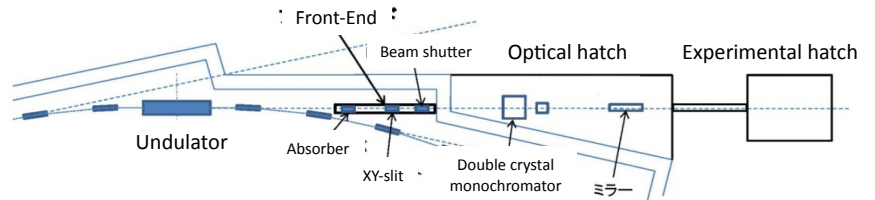


@400mA

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BEAMLINE

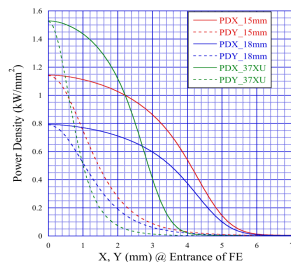
Front-End



- Expected maximum heat load is 10 kW/m.
ex. in SPring-8: Power density of short period undulator ~ 800 kW/mrad²

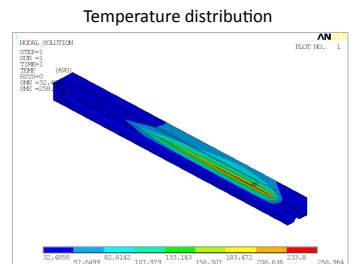
Virtual undulator

λ_u : 15 mm
 N_u : 290
 K_{max} : 2.3
 Total power: 26.7 kW
 Power density: 164.3 kW/mrad²



Absorber analysis

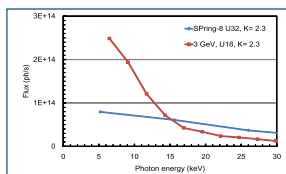
Model: SP8 standard
 Location: 10 m from source
 Irradiated power: 26.4 kW
 =>
 Light receiving surface: 259 °C
 Cooling surface: 89.6 °C
 =>
 SP8 standard absorber can receive radiation power of SLIT-J insertions



Double-crystal monochromator

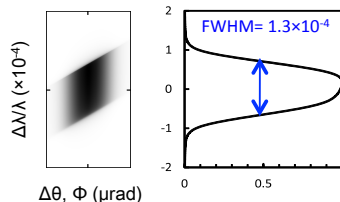
Si111 crystal

$h\nu$: 3 – 30 keV
 θ_B : 4 – 45 °
 =>
 Band width (energy resolution)
 $\Delta E/E \sim 1.3 \times 10^{-4}$

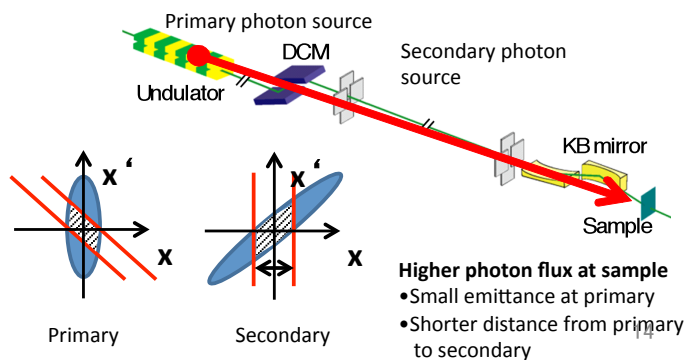


After Si111 monochromator

DuMond plot



Condenser mirror



Strategy

- Injector’s beam should be very low emittance for efficient injection to the ring.
- Achievement of XFEL machine, “**SACLA**”, allows us to construct a compact **full-energy injector linac**. (c-band technology, high brilliant thermionic gun . . .)
- **Soft-XFEL** will be considered to be a next step of SLIT-J as the advanced light source facility.

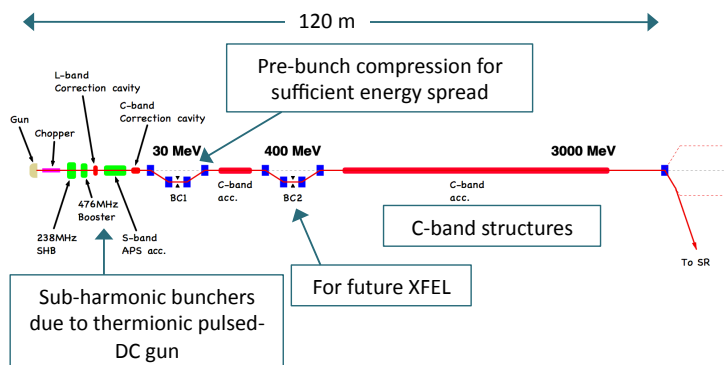
Target of injector linac

Beam energy	E	3 GeV
Energy spread	$\Delta E/E$	< 0.1 % (rms)
Energy stability	δE	< 0.1 % (rms)
Bunch charge	Q	~ 1 nC (max.)
Charge stability	δQ	~ 1 %
Transverse emittance	ϵ	< 5 mm.mrad* (normalized)
Bunch length	σ_z	< 5 ps
Repetition rate	f_{rep}	25 Hz (max.)

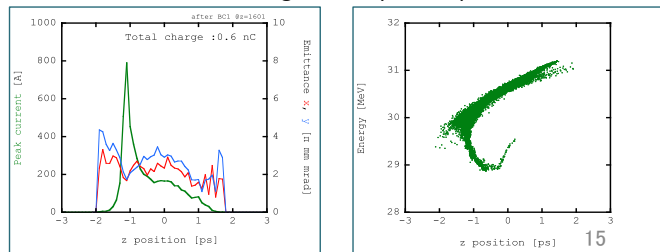
* 1 mm.mrad required for FEL

- Expected power consumption:
0.2 MW@1Hz, 1 MW@25H

Layout



Longitudinal phase space @ BC1

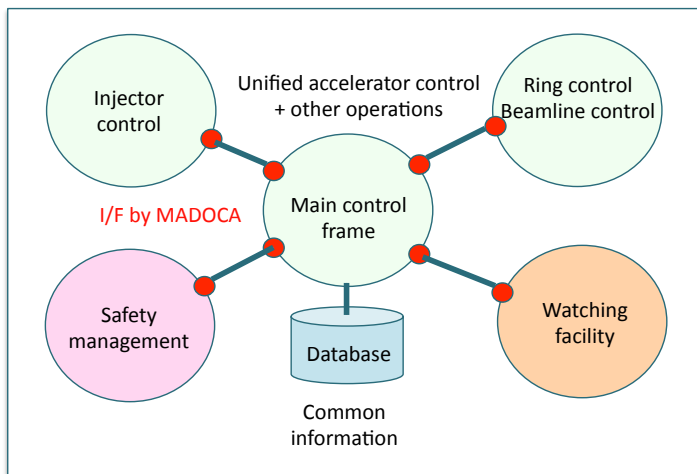


CONTROL and NETWORK

Mission

- Rapid construction of the system.
- Stable support for machine commissioning and tuning.
- Saving energy in operation.
- Reliable framework “MADCOA II” will be employed.

Integrated control system



Network structure

